

LONGITUDINALLY COUPLED RESONATOR TYPE SURFACE ACOUSTIC WAVE  
FILTER AND COMMUNICATION APPARATUS INCORPORATING THE SAME

BACKGROUND OF THE INVENTION

1. Field of the Invention

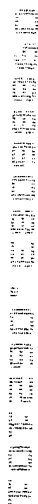
The present invention relates to longitudinally coupled resonator type surface acoustic wave filters. More particularly, the present invention relates to longitudinally coupled resonator type surface acoustic wave filters having balance-unbalance conversion functions.

2. Description of the Related Art

Recently, the sizes and weights of mobile phones have been greatly reduced. With such a trend, the numbers and sizes of components used in mobile phones have also been reduced while making such components more and more multifunctional.

With the above-described considerations, various kinds of mobile phones have been provided. In these mobile phones, surface acoustic wave filters are incorporated in the RF stages of the phones to have balance-unbalance conversion functions, or so-called balun functions.

Fig. 22 is a schematic plan view for illustrating the



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In such a surface acoustic wave filter having the balance-unbalance conversion function, regarding propagation characteristics in a pass band between the unbalanced signal terminal 108 and the balanced signal terminal 106 and between the unbalanced signal terminal 108 and the balanced terminal 107, amplitude characteristics need to be equal and propagating signals need to be 180° out of phase with

respect to each other. The condition in which the amplitude characteristics are equal is referred to as amplitude balance and the degree at which the propagating signals are 180° out of phase with respect to each other is referred to as phase balance.

The amplitude balance and the phase balance are defined as follows when the surface acoustic wave filter having the balance-unbalance conversion function is regarded as a device having three ports, such as the unbalanced input terminal as port 1 and the balanced output terminals as ports 2 and 3.

$$\text{Amplitude balance} = |A|.$$

$$A = |20\log S_{21}| - |20\log S_{31}|.$$

$$\text{Phase balance} = |B - 180|.$$

$$B = |\angle S_{21} - \angle S_{31}|.$$

In this definition,  $S_{21}$  denotes a transfer factor from the port 1 to the port 2 and  $S_{31}$  denotes a transfer factor from the port 1 to the port 3.

Ideally, in the pass band of the filter, the amplitude balance needs to be 0 dB and the phase balance needs to be 0°. However, with the use of the structure shown in Fig. 22, when intending to obtain a filter having a balance-unbalance conversion function, since the IDT 102 has an odd number of electrode fingers, the number of electrode fingers connected to the balanced signal terminal 106 increases by one more

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According to a preferred embodiment of the present invention, a longitudinally coupled resonator type surface acoustic wave filter having a balance-unbalance conversion function includes a piezoelectric substrate, first, second and third IDTs arranged on the piezoelectric substrate in a surface acoustic wave propagating direction, the second IDT being positioned between the first and third IDTs and having



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an even number of electrode fingers.

According to another preferred embodiment of the present invention, a longitudinally coupled resonator type surface acoustic wave filter having a balance-unbalance conversion function includes first-stage and second-stage longitudinally coupled resonator surface acoustic wave filters longitudinally coupled to each other, each of the first-stage and second-stage filters having a piezoelectric substrate and first, second and third IDTs arranged on the piezoelectric substrate in a surface acoustic wave propagating direction, an unbalanced signal terminal connected to one end of the second IDT of the first-stage longitudinally coupled resonator surface acoustic wave filter, a first balanced signal terminal connected to one end of the second IDT of the second-stage longitudinally coupled resonator surface acoustic wave filter, a second balanced signal terminal connected to the other end of the second IDT of the second-stage filter, a first signal line connecting one end of the first IDT of the first-stage longitudinally coupled resonator surface acoustic wave filter and one end of the first IDT of the second-stage longitudinally coupled resonator surface acoustic wave filter, and a second signal line connecting one end of the third IDT of the first-stage longitudinally coupled resonator surface acoustic wave filter and one end of the

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Fig. 7 shows a schematic plan view for illustrating a longitudinally coupled resonator type surface acoustic wave filter as a second modified example of the first preferred

embodiment of the present invention;

Fig. 8 shows a schematic plan view for illustrating a longitudinally coupled resonator type surface acoustic wave filter as a third modified example of the first preferred embodiment of the present invention;

Fig. 9 shows a schematic plan view for illustrating a longitudinally coupled resonator type surface acoustic wave filter as a fourth modified example of the first preferred embodiment of the present invention;

Fig. 10 shows a schematic plan view for illustrating a longitudinally coupled resonator type surface acoustic wave filter as a fifth modified example of the first preferred embodiment of the present invention;

Fig. 11 shows a schematic plan view for illustrating a longitudinally coupled resonator type surface acoustic wave filter according to a second preferred embodiment of the present invention;

Fig. 12 shows a schematic plan view for illustrating a surface acoustic wave filter as a modified example of the second preferred embodiment of the present invention;

Fig. 13 shows a graph illustrating the relationship between amplitude balance and frequency characteristics of each of the second preferred embodiment and the conventional device;

Fig. 14 shows a graph illustrating the relationship

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between phase balance and frequency characteristics of each of the second preferred embodiment and the conventional device;

Fig. 15 shows a schematic plan view for illustrating the conventional filter prepared for a comparison with the second preferred embodiment of the present invention;

Fig. 16 shows a schematic plan view for illustrating another modified example of the second preferred embodiment of the present invention;

Fig. 17 shows a schematic plan view for illustrating a longitudinally coupled resonator type surface acoustic wave filter according to a third preferred embodiment of the present invention;

Fig. 18 shows a graph illustrating the relationship between amplitude balance and frequency characteristics of each of the third preferred embodiment of the present invention and the conventional device;

Fig. 19 shows a graph illustrating the relationship between phase balance and frequency characteristics of each of the third preferred embodiment of the present invention and the conventional device;

Fig. 20 shows a schematic plan view for illustrating a longitudinally coupled resonator type surface acoustic wave filter according to a fourth preferred embodiment of the present invention;

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Fig. 21 shows a schematic block diagram for illustrating a communication apparatus as an example of an apparatus including the longitudinally coupled resonator type surface acoustic wave filter according to preferred embodiments of the present invention;

Fig. 22 shows a schematic plan view for illustrating the conventional longitudinally coupled resonator type surface acoustic wave filter.

#### DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

With reference to the drawings, the present invention will be clarified by describing preferred embodiments of a longitudinally coupled resonator type surface acoustic wave filter according to the present invention.

Fig. 1 shows a schematic plan view for illustrating the longitudinally coupled resonator type surface acoustic wave filter, preferably for use as a PCS reception filter, according to a first preferred embodiment of the present invention. In a longitudinally coupled resonator type surface acoustic wave filter 200, there is provided an electrode structure shown in Fig. 1 on a piezoelectric substrate 200A. A  $40 \pm 5^\circ$  Y-cut X-propagation  $\text{LiTaO}_3$  substrate is preferably used as the piezoelectric substrate 200A.

On the piezoelectric substrate, first, second and third



The number of the electrode fingers of IDT 202 = 40.

IDT wavelength  $\lambda I = 2.03 \mu m$ .

The wavelength  $\lambda R$  of each of reflectors 204 and 205 =  $2.05 \mu m$ .

The number of the electrode fingers of each of the reflectors 204 and 205 = 100.

IDT Gap =  $0.77 \lambda I$ . In this case, the gap between the IDTs is preferably substantially equivalent to a distance between the centers of the mutually adjacent electrode fingers of the IDTs.

IDT-reflector gap =  $0.55 \lambda R$ . The gap between an IDT and a reflector is preferably substantially equivalent to a distance between the centers of the mutually adjacent electrode fingers of the IDT and the reflector.

IDT Duty = 0.60.

Reflector Duty = 0.60.

Electrode-film thickness =  $0.08 \lambda I$ .

In addition, as shown in Fig. 1, the widths of the electrode fingers 206 and 207 on each side of the IDT 202 are preferably broader than those of the remaining electrode fingers. With this arrangement, the space in the gap between the IDTs is reduced.

As the characteristics of the first preferred embodiment of the present invention, the total number of the electrode fingers of the IDT 202 arranged in the center is

preferably an even number and an electrode finger 201a of the IDT 201 adjacent to the IDT 202 is arranged to define a signal electrode, whereas an electrode finger 203a of the IDT 203 adjacent to the IDT 202 is arranged to define a ground electrode. As shown here, of the electrode fingers of the right IDT 201 and the left IDT 203, the electrode fingers 201a and 203a adjacent to the central second IDT 202 have opposite polarities. The reason for this will be described below with reference to Figs. 2 and 3.

In the conventional longitudinally coupled resonator type surface acoustic wave filter 100 shown in Fig. 22, when one of the electrode fingers of the central IDT 102 is removed, as shown in Fig. 2, the number of the electrode fingers of the central IDT 102A is an even number. On the other hand, since a distance A between the IDT 102A and the IDT 103 is increased by about  $0.5 \lambda$ , loss due to the irradiation of a bulk wave is increased.

Thus, as shown in Fig. 3, there can be considered a structure in which the third IDT 103 is shifted by about  $0.5 \lambda$  toward the IDT 102A. However, in the structure shown in Fig. 3, the IDT 101 and the IDT 103 are  $180^\circ$  out of phase with each other.

Therefore, in this preferred embodiment of the present invention, as shown in Fig. 1, by having the IDT 201 reversed from the IDT 203, the IDT 201 and the IDT 203 are

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in phase with each other.

Fig. 4 shows a graph illustrating the relationship between amplitude balance and frequencies in the longitudinally coupled resonator type surface acoustic wave filter according to the first preferred embodiment of the present invention. Fig. 5 shows a graph illustrating the relationship between phase balance and frequencies in the same filter. In Figs. 4 and 5, solid lines show the results of the first preferred embodiment of the present invention. In addition, for comparison, in Figs. 4 and 5, broken lines show the characteristics of the conventional filter shown in Fig. 22.

In this case, the conventional filter has the same detailed design as that of the first preferred embodiment, except that one of the electrode fingers of the central IDT in the conventional filter is removed.

A pass-band frequency range used in the PCS reception filter is between about 1930 MHz to about 1990 MHz. As seen in Fig. 4, in the frequency band range, the maximum amplitude balance is 3.2 dB in the conventional filter, whereas it is about 2.7 dB in the first preferred embodiment of the present invention. That is, the amplitude balance is improved by about 0.5 dB in this preferred embodiment of the present invention. Moreover, as shown in Fig. 5, whereas the maximum phase balance in the conventional filter is 21°,

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the maximum phase balance in the first preferred embodiment of the present invention is about  $17^\circ$ . That is, obviously, the phase balance is improved by about  $4^\circ$  in this preferred embodiment of the present invention.

As mentioned above, in this preferred embodiment of the present invention, the total number of the electrode fingers of the central second IDT 202 is an even number and the polarity of the electrode finger of the first IDT 201 adjacent to the central second IDT 202 is reversed from the polarity of the electrode finger of the third IDT 203 adjacent to the IDT 202. Thus, as compared with the conventional filter, obviously, the first preferred embodiment of the present invention provides a longitudinally coupled resonator type surface acoustic wave filter having a balance-unbalance conversion function, in which the amplitude balance and the phase balance are both greatly improved.

This preferred embodiment preferably uses a  $40 \pm 5^\circ$  Y-cut X-propagation  $\text{LiTaO}_3$  substrate. However, the substrate used in the present invention is not restricted to the  $\text{LiTaO}_3$  substrate. Any other piezoelectric substrate may be used such as a  $64$  to  $72^\circ$  Y-cut X-propagation  $\text{LiNbO}_3$  substrate or a  $41^\circ$  Y-cut X-propagation  $\text{LiNbO}_3$  substrate, for example. Other suitable substrates may also be used.

In addition, in the first preferred embodiment of the

present invention, a balanced signal is obtained from the central second IDT. However, as shown in Fig. 6, the balanced signal may be obtained from each of the first IDT 201 and the third IDT 203 on each side of the central IDT 202. In Fig. 6, terminals 213 and 214 are balanced signal terminals connected to the first and third IDTs 201 and 203, respectively, and a terminal 215 is an unbalanced signal terminal connected to the central second IDT 202.

Fig. 7 shows a schematic plan view for illustrating the electrode structure of another modified example of the first preferred embodiment of the present invention. As shown in Fig. 7, a surface acoustic wave resonator 216 may be connected between the first and third IDTs 201 and 203 and a terminal 212.

Fig. 8 shows a schematic plan view for illustrating the electrode structure of another modified example of the first preferred embodiment of the present invention. In a longitudinally coupled resonator type surface acoustic wave filter 217 shown in Fig. 8, the longitudinally coupled resonator type surface acoustic wave filters 200 according to the first preferred embodiment are longitudinally connected in a two-stage structure.

In addition, Fig. 9 shows a schematic plan view for illustrating a longitudinally coupled resonator type surface acoustic wave filter as another modified example of the



first preferred embodiment of the present invention. In Fig. 9, the longitudinally coupled resonator type surface acoustic wave filter 200 of the first preferred embodiment is longitudinally connected to a 3-IDT-type longitudinally coupled resonator type surface acoustic wave filter 219 including the central IDT 218 having an odd number of electrode fingers. In other words, in the multi-stage longitudinally coupled resonator type surface acoustic wave filters, even when at least only one-stage filter is defined by the longitudinally coupled resonator type surface acoustic wave filter 200 of the first preferred embodiment, as in the first preferred embodiment, greatly improved amplitude and phase balances are achieved.

Fig. 10 shows a schematic plan view for illustrating the electrode structure of another modified example of the longitudinally coupled resonator type surface acoustic wave filter of the first preferred embodiment. In a longitudinally coupled resonator type surface acoustic wave filter 220 shown in Fig. 10, narrow pitch electrode finger sections N1 to N4 are disposed in first, second and third IDTs 221, 222 and 223. Specifically, in the IDT 221, the narrow pitch electrode finger section N1, is arranged such that the electrode finger pitches of some portions from the end portion of the IDT 222 are narrower than the electrode finger pitches of the remaining portions of the IDT 221.

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Similarly, on each end portion of the IDT 222, the narrow pitch electrode finger sections N2 and N3 are provided. In addition, in the IDT 223, on the side adjacent to the IDT 222, the narrow pitch electrode finger section N4 is provided. As shown here, in the regions where the IDTs are adjacent to each other, even when disposing the narrow pitch electrode finger sections having relatively narrow electrode finger pitches, by arranging the remaining portions like the first preferred embodiment, greatly improved amplitude and phase balances are achieved.

Fig. 11 shows a schematic plan view for illustrating the electrode structure of a longitudinally coupled resonator type surface acoustic wave filter according to a second preferred embodiment of the present invention.

The second preferred embodiment of the present invention relates to an AMPS reception filter.

Similar to the first preferred embodiment, the electrode structure shown in Fig. 11 is preferably formed on a  $40 \pm 5^\circ$  Y-cut X-propagation  $\text{LiTaO}_3$  substrate to constitute a longitudinally coupled resonator type surface acoustic wave filter 300 of the second preferred embodiment of the present invention.

In the longitudinally coupled resonator type surface acoustic wave filter 300, a first longitudinally coupled resonator type surface acoustic wave filter 301 and a second

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longitudinally coupled resonator type surface acoustic wave filter 302 are longitudinally connected to each other. The first and second longitudinally coupled resonator type surface acoustic wave filters 301 and 302 preferably have the same structure.

Similar to the first preferred embodiment, the first-stage longitudinally coupled resonator type surface acoustic wave filter 301 includes first, second and third IDTs 303, 304 and 305 arranged in a surface acoustic wave propagating direction and reflectors 306 and 307, and the second-stage longitudinally coupled resonator type surface acoustic wave filter 302 includes first, second and third IDTs 308, 309 and 310 in the surface acoustic wave propagating direction and reflectors 311 and 312. The reflectors 306, 307, 311, and 312 are disposed on the right and left sides of the regions where the IDTs of the filters 301 and 302 are arranged. One end of each of the first and third IDTs 303 and 305 of the first longitudinally coupled resonator type surface acoustic wave filter 301 is connected to one end of each of the first and third IDTs 308 and 310 of the second longitudinally coupled resonator type surface acoustic wave filter 302 via first and second signal lines 316 and 317. One end of the IDT 304 is connected to a terminal 313. One end of the IDT 309 is connected to a terminal 314 and the other end thereof is connected to a terminal 315. The

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remaining ends of the IDTs 303, 304 and 305 and 308, 309 and 310 are connected to ground potentials.

The terminals 314 and 315 are balanced signal terminals. The terminal 313 is an unbalanced signal terminal. The detailed design of an example of the filter 300 will be presented below.

Electrode finger cross width  $W = 49.0 \lambda_l$ .

The number of the electrode fingers of first IDTs 303 and 308 = 24.

The number of the electrode fingers of second IDTs 304 and 309 = 34.

The number of the electrode fingers of third IDTs 305 and 310 = 25.

IDT wavelength  $\lambda_l = 4.49 \mu\text{m}$ .

Reflector wavelength  $\lambda_R = 4.64 \mu\text{m}$ .

The number of reflector electrode fingers = 120.

IDT gap =  $0.79 \lambda_l$ .

IDT-reflector gap =  $0.47 \lambda_R$ .

IDT duty = 0.73.

Reflector duty = 0.55.

Electrode film thickness =  $0.08 \lambda_l$ .

In this preferred embodiment of the present invention, the widths of the electrode fingers 304a, 304b, 309a, and 309b on each end of the central second IDTs 304 and 309 are broadened to reduce spaces between the adjacent IDTs.

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In this preferred embodiment, the number of the electrode fingers of each of the IDTs 304 and 309 is preferably an even number as in the case of the first preferred embodiment. In addition, the electrode fingers 303a and 305a of the IDTs 303 and 305 adjacent to the IDT 304 and the electrode fingers 308a and 310a of the IDTs 308 and 310 adjacent to the IDT 309 are arranged to define ground electrodes.

In the first longitudinally coupled resonator type surface acoustic wave filter 301, the IDTs 303 and 305 are  $180^\circ$  out of phase with the IDT 304. Thus, when the IDTs 303 and 305 are connected in parallel to make the single stage filter, it is impossible to obtain filter characteristics. However, simultaneously, in the second longitudinally coupled resonator type surface acoustic wave filter 302, the IDTs 308 and 310 are also  $180^\circ$  out of phase with the IDT 309. As a result, since surface waves propagating from the IDTs 308 and 310 to the IDT 309 are in phase with each other, filter characteristics can be obtained by connecting the first and second longitudinally coupled resonator type surface acoustic wave filters 301 and 302. In other words, an electric signal propagating through a first signal line 316 is  $180^\circ$  out of phase with an electric signal propagating through a second signal line 317.

Fig. 13 shows the relationship between amplitude

balance and frequencies in the second preferred embodiment of the present invention. Fig. 14 shows the relationship between phase balance and frequencies. In Figs. 13 and 14, solid lines indicate the results of the second preferred embodiment and broken lines indicate the results of a conventional device shown in Fig. 15, which is prepared for comparison.

In a conventional longitudinally coupled resonator type surface acoustic wave filter 401 shown in Fig. 15, the numbers of the electrode fingers of first, second and third IDTs 402, 403 and 404 are preferably the same as those of the second preferred embodiment, except that the number of the electrode fingers of the first IDT is preferably 24, the number of the electrode fingers of the second IDT is preferably 35, and the number of the electrode fingers of the third IDT is preferably 24.

A pass-band frequency range in the AMPS reception filter is between approximately 860 MHz and approximately 894 MHz.

In the frequency range, the maximum amplitude balance is 1.9 dB in the conventional filter, whereas it is about 0.9 dB in the second preferred embodiment of the present invention. Thus, obviously, the amplitude balance is improved by about 1.0 dB in the second preferred embodiment.

In addition, whereas the maximum phase balance is  $17^\circ$

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in the conventional filter, it is about  $8^\circ$  in the second preferred embodiment. The phase balance is improved by about  $9^\circ$  in the second preferred embodiment of the present invention.

As mentioned above, the reason that the amplitude and phase balances are improved is as follows. The second IDT has an even number of electrode fingers and the electric signal propagating through the first signal line 316 is  $180^\circ$  out of phase with the electric signal propagating through the second signal line 317. As a result, the electrode fingers of the first and third IDTs adjacent to the central second IDT can be both arranged to define ground electrodes, and a distance B (see Fig. 11) between the electrode finger 309a connected to the terminal 315 and the electrode signal finger 308b of the IDT 308 is substantially equal to a distance C (see Fig. 11) between the electrode finger 309b connected to the terminal 314 and the signal electrode finger 310b of the IDT 310. In contrast, in the conventional device shown in Fig. 15, distances D and E between electrode fingers, specified in the figure, between the adjacent IDTs in the second longitudinally coupled resonator type surface acoustic wave filter are differentiated by about  $0.5 \lambda$ .

In the second preferred embodiment, the electrode fingers of the right first IDT and the left third IDT

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adjacent to the second IDT are ground electrodes. However, even when these electrode fingers constitute signal electrodes, the same advantages can be obtained.

As mentioned above, in the second preferred embodiment, the first and second longitudinally coupled resonator type surface acoustic wave filters 301 and 302 including the second IDTs having the even number of electrode fingers are longitudinally connected in the two-stage structure. Additionally, the electric signal propagating through the first signal line 316 is 180° out of phase with the electric signal propagating through the second signal line 317. With this arrangement, the polarity of the electrode fingers of the central second IDT can be the same as the polarities of the electrode fingers of the first and third IDTs adjacent to the second IDT. Both of the amplitude balance and the phase balance are also greatly improved.

Also, in the case where narrow pitch electrode fingers are used at the portion where two IDTs are adjacent to each other in the structure shown in Fig. 11, with respect to the second preferred embodiment, as shown in Fig. 10, the characteristics which indicates improved balance can be obtained.

Fig. 12 shows a schematic plan view for illustrating a modified example of the second preferred embodiment of the present invention. This modified example is differentiated





that the electrode fingers of the interdigital electrode 322a are interdigitated with the electrode fingers of the interdigital electrodes 322b and 322c. In other words, one of a pair of the interdigital electrodes defining the second IDT 322 is split into the two interdigital electrodes 322b and 322c, which are connected to balanced signal terminals 314 and 315. In this case, in the first-stage longitudinally coupled resonator type surface acoustic wave filter 301, the IDT 303 is  $180^\circ$  out of phase with the IDT 305. In the second-stage longitudinally coupled resonator type surface acoustic wave filter 321, the first IDT 308 is  $180^\circ$  out of phase with the second IDT 310. With this arrangement, an electric signal propagating through a signal line 316 is  $180^\circ$  out of phase with an electric signal propagating through a signal line 317. Thus, the polarities of the electrode fingers of the IDT 308 and the IDT 310 adjacent to the IDT 322 are the same. As a result, the amplitude and phase balances in this filter are greatly improved as with the second preferred embodiment of the present invention.

Fig. 17 shows a schematic plan view for illustrating the electrode structure of a longitudinally coupled resonator type surface acoustic wave filter according to a fourth preferred embodiment of the present invention.

A longitudinally coupled resonator type surface

acoustic wave filter 600 of the fourth preferred embodiment preferably has the same structure as that of the second preferred embodiment, except for the following points.

In this preferred embodiment, in first-stage and second-stage longitudinally coupled resonator type surface acoustic wave filters 601 and 602, the numbers of the electrode fingers of first, second and third IDTs are determined, in which the number of the electrode fingers of each of the first IDTs 603 and 608 is preferably 24, the number of the electrode fingers of each of the second IDTs 604 and 609 is preferably 35, and the number of the electrode fingers of each of the third IDTs 605 and 610 is preferably 24.

In the fourth preferred embodiment, characteristically, the polarity of an electrode finger 603a of the first IDT 603 adjacent to the IDT 604 is opposite to the polarity of an electrode finger 605a of the third IDT 605 adjacent to the IDT 604. In addition, the polarity of an electrode finger 608a of the first IDT 608 adjacent to the IDT 609 is opposite to an electrode finger 610a of the third IDT 610 adjacent to the IDT 609.

When considering only the first-stage longitudinally coupled resonator type surface acoustic wave filter 601, each of the IDTs 603 and 605 is 180° out of phase with the IDT 604. Thus, it is impossible to obtain filter

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Additionally, as shown in Fig. 19, whereas the maximum phase balance is  $17^\circ$  in the conventional filter, it is about  $11^\circ$  in the fourth preferred embodiment. Thus, the phase balance is improved by about  $6^\circ$  in the fourth preferred embodiment.

In other words, in the fourth preferred embodiment, the first-stage and first-stage longitudinally coupled resonator type surface acoustic wave filters having three IDTs are longitudinally connected to each other. In addition, the polarities of the electrode fingers of the first and third IDTs adjacent to the central second IDT are opposite to each other. With this arrangement, the amplitude balance and the phase balance are greatly improved.

Fig. 20 shows a schematic plan view for illustrating the electrode structure of the longitudinally coupled resonator type surface acoustic wave filter according to a fifth preferred embodiment of the present invention. The fifth preferred embodiment uses 3-IDT-type longitudinally coupled resonator type surface acoustic wave filters 901, 902, 903 and 904 having first, second and third IDTs. In each of the longitudinally coupled resonator type surface acoustic wave filters 901, 902, 903 and 904, the central second IDT has even electrode fingers, and the polarities of the electrode fingers of the right and left IDTs adjacent to the central second IDT are the same. For example, in the longitudinally coupled resonator type surface acoustic wave

2025 RELEASE UNDER E.O. 14176

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	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100	2101	2102	2103	2104	2105	2106	2107	2108	2109	2110	2111	2112	2113	2114	2115	2116	2117	2118	2119	2120	2121	2122	2123	2124	2125	2126	2127	2128	2129	2130	2131	2132	2133	2134	2135	2136	2137	2138	2139	2140	2141	2142	2143	2144	2145	2146	2147	2148	2149	2150	2151	2152	2153	2154	2155	2156	2157	2158	2159	2160	2161	2162	2163	2164	2165	2166	2167	2168	2169	2170	2171	2172	2173	2174	2175	2176	2177	2178	2179	2180	2181	2182	2183	2184	2185	2186	2187	2188	2189	2190	2191	2192	2193	2194	2195	2196	2197	2198	2199	2200	2201	2202	2203	2204	2205	2206	2207	2208	2209	2210	2211	2212	2213	2214	2215	2216	2217	2218	2219	2220	2221	2222	2223	2224	2225	2226	2227	2228	2229	2230	2231	2232	2233	2234	2235	2236	2237	2238	2239	2240	2241	2242	2243	2244	2245	2246	2247	2248	2249	2250	2251	2252	2253	2254	2255	2256	2257	2258	2259	2260	2261	2262	2263	2264	2265	2266	2267	2268	2269	2270	2271	2272	2273	2274	2275	2276	2277	2278	2279	2280	2281	2282	2283	2284	2285	2286	2287	2288	2289	2290	2291	2292	2293	2294	2295	2296	2297	2298	2299	2300	2301	2302	2303	2304	2305	2306	2307	2308	2309	2310	2311	2312	2313	2314	2315	2316	2317	2318	2319	2320	2321	2322	2323	2324	2325	2326	2327	2328	2329	2330	2331	2332	2333	2334	2335	2336	2337	2338	2339	2340	2341	2342	2343	2344	2345	2346	2347	2348	2349	2350	2351	2352	2353	2354	2355	2356	2357	2358	2359	2360	2361	2362	2363	2364	2365	2366	2367	2368	2369	2370	2371	2372	2373	2374	2375	2376	2377	2378	2379	2380	2381	2382	2383	2384	2385	2386	2387	2388	2389	2390	2391	2392	2393	2394	2395	2396	2397	2398	2399	2400	2401	2402	2403	2404	2405	2406	2407	2408	2409	2410	2411	2412	2413	2414	2415	2416	2417	2418	2419	2420	2421	2422	2423	2424	2425	2426	2427	2428	2429	2430	2431	2432	2
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[illegible]

coupled resonator type surface acoustic wave filter according to other preferred embodiments of the present invention.

In Fig. 21, an antenna 61 is connected to a duplexer 62. A surface acoustic wave filter 64 and an amplifier 65 are connected between the duplexer 62 and a mixer 63 of the reception section. An amplifier 67 and a surface acoustic wave filter 68 are connected between the duplexer 62 and a mixer 66 of the transmission section. As shown here, when the amplifier 65 is adapted to a balanced signal, the longitudinally coupled resonator type surface acoustic wave filter of various preferred embodiments of the present invention can be suitably used as the surface acoustic wave filter 64.

As described above, in the longitudinally coupled resonator type surface acoustic wave filter according to various preferred embodiments of the present invention, the central second IDT preferably has an even number of electrode fingers. In addition, the polarities of electrode fingers adjacent to the second IDT in the first and third IDTs disposed on the right-and-left sides of the second IDT are opposite. Thus, the amplitude balance and the phase balance between the balanced signal terminals are greatly effectively improved. As a result, preferred embodiments of the present invention provide a surface acoustic wave filter

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having an excellent balance-unbalance conversion function.

Furthermore, in the longitudinally coupled resonator type surface acoustic wave filter according to other preferred embodiments of the present invention, first-stage and second-stage longitudinally coupled resonator type surface acoustic wave filters having first, second and third IDTs are longitudinally connected to each other. One end of the second IDT of the first-stage longitudinally coupled resonator type surface acoustic wave filter is connected to an unbalanced signal terminal. Additionally, both ends of the second IDT of the second-stage longitudinally coupled resonator type surface acoustic wave filter are connected to a pair of balanced signal terminals. In this arrangement, an electric signal propagating through a first signal line connecting one end of the first IDT of the first-stage longitudinally coupled resonator type surface acoustic wave filter and one end of the first IDT of the second-stage longitudinally coupled resonator type surface acoustic wave filter is 180° out of phase with an electric signal propagating through a second signal line connecting one end of the third IDT of the first-stage longitudinally coupled resonator type surface acoustic wave filter and one end of the third IDT of the second-stage longitudinally coupled resonator type surface acoustic wave filter. As a result, the polarity of the electrode finger of the second IDT

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While the present invention has been described with reference to what are at present considered to be preferred embodiments, it is to be understood that various changes and modifications may be made thereto without departing from the

